

Theory of Electroporation of Planar Bilayer Membranes: Predictions of the Aqueous Area, Change in Capacitance, and Pore-Pore Separation

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ABSTRACT A large increase in the transmembrane voltage, $U(t)$, of a fluid bilayer membrane is believed to result in the occurrence of temporary aqueous pathways ("pores") across the membrane. The number, size, and evolution dynamics of these pores are expected to be crucial to the transport of water-soluble species ranging from small ions to macromolecules such as proteins and nucleic acids. In this paper we use a transient aqueous pore theory to estimate the fraction of the membrane area, $F_w(t)$, which is temporarily occupied by water-filled pores for short square, exponential, and bipolar square pulses. For short pulses, "reversible electrical breakdown" occurs when the transmembrane voltage reaches about 1 V, and $F_w(t)$ is predicted to rise rapidly, but always to be less than 10^{-3} . The conductance of a large number of pores causes reversible electrical breakdown and prevents a significantly larger U from being reached. Despite the large dielectric constant of water, for reversible electroporation the associated change in membrane capacitance, ΔC , due to the pores is predicted to be small. Moreover, for a flat membrane the minimum value of the mean pore-pore separation is large, about 60 times the minimum pore radius. In flat membranes, pores are predicted to repel, but the opposite is expected for curved cell membranes, allowing the possibility of coalescence in cell membranes. For some moderate values of U , rupture (irreversible electrical breakdown) occurs, as one or more supracritical pores expand to the membrane boundary and the entire membrane area becomes aqueous. In all cases it is found that a quantitative description of electroporation requires that a pore size distribution, rather than a single size pore.

INTRODUCTION

Electroporation is increasingly used for the introduction of water-soluble molecules into cells and has many potential applications in biology and medicine (Neumann et al., 1989; Tsong, 1991; Chang et al., 1992; Blank, 1993; Weaver, 1993a, b; Orlowski and Mir, 1993). Although the mechanism by which this occurs is incompletely understood, it is generally believed that a rapid structural rearrangement of the membrane occurs, whereby many aqueous pathways ("pores") perforate the membrane. One class of electroporation theories is based on transient aqueous pores that are explicitly assumed to be created by the combined effects of thermal fluctuations and the local electric field across the membrane. The first version of transient aqueous pore theories was presented by Chizmadzhev and co-workers in a series of seven back-to-back papers, of which only the first is cited here (Abidor et al., 1979). In the present paper we estimate the extent of membrane poration by using a recent version of a transient aqueous pore

theory (Barnett and Weaver, 1991). This allows estimation of the total aqueous area (expressed here as a fraction, F_w), the change in membrane capacitance due to the pores, and the mean separation between the pores. The latter is relevant to the possibility that pores coalesce to form "cracks" or other larger openings in the membrane (Sugar et al., 1987).

Planar bilayer membranes have often been used to investigate basic aspects of the lipid bilayer component of cell membranes. In the case of cell membrane electroporation, it is likely that most of the poration is localized to the relatively small region for which the transmembrane voltage, $U(t)$, is largest. For example, in the case of an isolated spherical cell, electroporation is believed to occur mainly at the "polar caps" of the cell. Indeed, there is experimental support for this, based on fluorescence measurements that respond to the local transmembrane voltage (Hibino et al., 1991). It is plausible, therefore, that such local regions can be reasonably approximated by sections of planar membrane that experience the same $U(t)$, and this further motivates the present study.

MATERIALS AND METHODS

We have slightly modified a previous theoretical model (Barnett and Weaver, 1991; Weaver and Barnett, 1992) by rewriting the computer code to provide greater flexibility in what can be computed. As a consequence, simulation of electroporation due to an exponential pulse or bipolar square pulse in addition to a square pulse was made possible. We then carried out several calculations of electrical behavior, the dynamic, heterogeneous pore population, and quantities dependent on the pore population. A detailed

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presentation of the basic model (Barnett and Weaver, 1991; Weaver and Barnett, 1992) is too lengthy to include here. Key features are briefly described, the Appendix provides a discussion of the origin of some of the parameters, and a complete listing of the notation and the values of fixed parameters is given in Table 1.

We begin with the estimate of the free energy change, ΔE , associated with forming a pore of radius r if the spatially averaged transmembrane voltage is $U(t)$:

$$\Delta E(r, U) = 2\pi\gamma r - \pi\Gamma r^2 - \frac{\pi(K_w - K_l)U^2}{h} \int_{r_{\min}}^r \alpha^2 r dr, \quad (1)$$

where the effects of inhomogeneous electric fields near the pore entrances, Born energy repulsion of ions, and hindered drift motion within the pore are subsumed into the function $\alpha(r)$

$$\alpha(r) = \left[1 + \frac{\pi\sigma_p(r)}{2h\sigma_e} \right]^{-1}. \quad (2)$$

Here σ_p is the reduced conductivity within a pore, and σ_e is the bulk solution conductivity. The appearance of a heterogeneous pore population in response to the occurrence of elevated U is governed by a phenomenological estimate of the pore creation rate

$$(\dot{N})_c = \nu_0 V_m \exp\left(-\frac{\delta_c - aU^2}{kT}\right). \quad (3)$$

Here $\nu = \nu_0$, V_m is the attempt rate, ν_0 is an attempt rate density, and $V_m = hA_m$ is the membrane volume (Weaver and Mintzer, 1981). Although not understood in detail, it is assumed that an energy barrier, $\Lambda = \delta_c - aU^2$, must

TABLE 1 Notation and values of parameters

Parameter		Value
a	coefficient of U^2 in Λ	1.9×10^{-20} F
A_m	Membrane area ($\pi R_{\text{aperture}}^2$)*	1.45×10^{-6} m ²
C_0	C, the capacitance of membrane at $U = 0$	9.61×10^{-9} F
D_p	Diffusion constant in pore radius space*	5×10^{-14} m ² s ⁻¹
$G(t)$	Membrane conductance	Initially almost zero
h	Membrane thickness*	2.8 nm
kT	Boltzmann's constant times temperature	4×10^{-21} J
K_l	Dielectric constant of lipid*	2.1
K_w	Dielectric constant of water	80
R_E	Series resistance of electrolyte, electrodes, and wires	30 Ω
R_N	Internal resistance of current source (pulse generator)	50 Ω
$R(t)$	Membrane resistance ($1/G(t)$)	Initially almost infinite
r_{\max}	Large pore initial size	40 nm
r_{\min}	Minimum pore radius*	1 nm
γ	Pore edge energy density*	2×10^{-11} J m ⁻¹
Γ	Membrane surface energy*	1×10^{-3} J m ⁻²
δ_c	Voltage-independent barrier to pore formation*	2×10^{-19} J
δ_d	Pore destruction energy barrier*	2×10^{-19} J
ϵ_0	Permittivity of free space	8.85×10^{-12} F m
Δr	Numerical grid spacing of simulation	0.026 nm
χ	Pore destruction rate prefactor*	5×10^{16} m s ⁻¹
ν	Pore creation rate prefactor*	10^{28} s ⁻¹
σ_e	Conductivity of bulk solution	9.8 S m ⁻¹

* Parameters characterizing the membrane. Many features of the basic model and its parameters have been published previously (Barnett and Weaver, 1991).

be overcome to form a pore. Other estimates of the barrier (Glaser et al., 1988) could be incorporated in future versions, but to maintain consistency with our previous work (Barnett and Weaver, 1991), the previously employed barrier is again used here. Pores are also assumed to disappear, but are destroyed only when they shrink to their minimum allowed radius, r_{\min} . The destruction process is assumed to be independent of U . Specifically, the total rate of pore destruction is

$$(\dot{N})_d = \chi n(r_{\min}) \exp\left(-\frac{\delta_d}{kT}\right), \quad (4)$$

where δ_d is a fixed barrier, and χ (Table 1) is a constant with dimensions of velocity. Once pores have formed their expansion and contraction is governed by Smoluchowski's equation

$$\frac{\partial n}{\partial t} = D_p \left(\frac{\partial^2 n}{\partial r^2} + \frac{\partial}{\partial r} \left(\frac{n}{kT} \frac{\partial \Delta E}{\partial r} \right) \right) \quad (5)$$

The function $n(r, t)$ is a pore probability density function, such that the instantaneous number of pores with radii between r and $r + \Delta r$ is $n(r, t)\Delta r$. This governs the evolution of $n(r, t)$, the pore probability density function, in response to changes in ΔE caused by a changing transmembrane voltage, $U(t)$, through Eq. 1 (Figs. 3, 7, and 11).

This differential equation is implicitly coupled to a first order differential equation that describes the interaction of the membrane with its environment, i.e., the charging of the membrane through the bathing electrolyte from the pulse generator (Fig. 1). After the pulse ends, the generator is disconnected from the system so that the membrane can then discharge only by moving ions across the membrane through pores (Figs. 2, 6, and 10).

$$C \frac{dU}{dt} = \begin{cases} \frac{1R_N}{R_E + R_N} - U \left(G(t) + \frac{1}{R_E + R_N} \right) & \text{if } t < t_{\text{pulse}} \\ -UG(t) & \text{if } t > t_{\text{pulse}} \end{cases} \quad (6)$$

Here I is the instantaneous current flowing through the membrane, which depends on the pore sizes, the local, decreased transmembrane voltages (because of the spreading resistance), and the reduced conductivity within the pores. Equations 3–6 together determine the evolution of the pore population and its electrical interaction with the membrane's environment. Other ingredients and inputs such as the physical models for pore conduction, the rates of pore creation and of pore destruction (at r_{\min}), and the pulse magnitude and shape then can be varied.

Both mechanical and electrical behavior are relevant. A planar membrane can rupture (mechanical destruction) by acquiring one or more supracritical pores (Abidor et al., 1979; Weaver and Mintzer, 1981; Sugar, 1981; Toner and Cravalho, 1990). Alternatively, a planar membrane can protect itself against rupture by rapidly acquiring so many small pores that a very large membrane conductance is achieved, which quickly discharges the membrane before any supracritical pores can evolve (Powell et al., 1986; Barnett and Weaver, 1991; Weaver and Barnett, 1992). The appearance of a heterogeneous pore population is fundamental to the transient aqueous pore model and is described by a pore probability density function, $n(r, t)$, which is obtained as a solution of Eq. 5 (Figs. 3, 7, and 11).

Partial insight into the pore population can be gained by considering the average pore radius, $\bar{r}(t)$, which is straightforwardly computed as

$$\bar{r}(t) = \frac{1}{N_p(t)} \int_{r_{\min}}^{\infty} r n(r, t) dr, \quad (7)$$

where the instantaneous total number of pores in the membrane is

$$N_p(t) = \int_{r_{\min}}^{\infty} n(r, t) dr. \quad (8)$$

Typical predicted behavior for short square, exponential, and bipolar square pulses is shown in Figs. 4, 8, and 12.

The total pore area at the midplane of the membrane is similarly estimated. In the transient aqueous pore theories to date, including the present version, a very simple, circular cylinder geometry has been used to represent

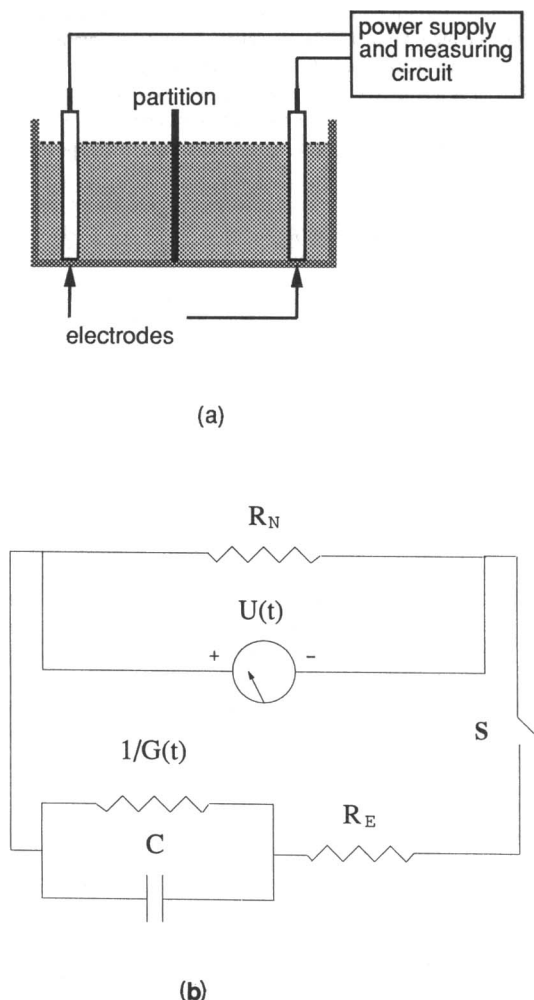


FIGURE 1 Equivalent circuit that represents the planar membrane and the external environment (experimental apparatus). The resistor, R_E , represents the combined resistance of (1) the bulk electrolyte separating the membrane from the electrodes, (2) any constant electrolyte/electrode interfacial resistance, and (3) the pulse generator output resistance. Conceptually, the generator develops a voltage, $V(t)$, which is applied to the membrane system by closing the switch, S . At the end of the pulse, the switch is instantaneously opened, so that the membrane can only discharge through the membrane. The membrane is represented by an essentially constant capacitance, C , and time-dependent resistance, $R(t)$. The membrane conductance, $G(t) = 1/R$, is attributed to the instantaneous sum of the conductances of all the individual transient pores. Consistent with this approach, the transient pore population is described by a probability density function, $n(r, t)$, which appears in Eq. 5, such that $n(r, t)\Delta r$ is the average number of pores with radii between r and $r + dr$ at time t . The instantaneous transmembrane voltage, $U(t)$, is described by Eq. 6. These general features are unchanged from the previous version of the theoretical model (Barnett and Weaver, 1991). The approximation that C is constant is here found to be consistent with the behavior of the present model, as was estimated in a much earlier model that treated the worst case of a membrane saturated with pores (Weaver et al., 1984).

a pore. Here the aqueous area, $A_w(t)$, of the membrane was estimated by computing the total cross sectional areas of the pores.

$$A_w(t) = \int_{r_{\min}}^{\infty} \pi r^2 n(r, t) dr \quad (9)$$

The total membrane area, $A_m = \pi R_{\text{aperture}}^2$, is considered to be the sum of lipid

area and aqueous area. As pores form in a planar membrane that exists across a macroscopic aperture, the excess membrane material is believed eventually to be transferred to the edge of the aperture. This interpretation is central to the idea that rupture occurs by expansion of one or more supercritical pores so that all of the membrane material reaches the aperture. When this occurs, the "membrane" is entirely aqueous, and is therefore regarded as destroyed. However, for short times transfer of membrane material over the distance $\approx R_{\text{aperture}}$ cannot be valid. Instead, local accumulation of material and local thickening of the membrane is a more likely immediate outcome of pore formation. In the spirit of an order of magnitude estimate, excess membrane material near a pore can be expected to remain localized for times less than $t_{\text{local}} \approx R_{\text{aperture}}/v_{\text{sound}}$. Here $v_{\text{sound}} \approx 1.5 \times 10^3 \text{ m s}^{-1}$ is estimated by using the speed of sound in water and in oil. For the membrane used here ($R_{\text{aperture}} \approx 7 \times 10^{-4} \text{ m}$), this gives $t_{\text{local}} \approx 5 \times 10^{-7} \text{ s}$, which is on the same time scale as REB. Thus, for times shorter than t_{local} , excess membrane material probably accumulates locally, resulting in locally thicker regions of the membrane. However, local thickening of portions of the lipid area of the membrane does not affect the aqueous area of the membrane due to pores. When expressed as an aqueous fractional area, $F_w(t)$, this is

$$F_w(t) = \frac{A_w(t)}{A_m} \quad (10)$$

The transient aqueous pore theories to date have assumed that the membrane capacitance, C , is constant (Fig. 1). One experimental observation of electroporation supports this (Chernomordik et al., 1982). Here this assumption is tested by estimating the change in C that is due to the appearance of the aqueous pores, i.e., by regarding each pore as a microscopic capacitor in which the relevant dielectric constant is that of bulk water ($K_w = 80$). This estimate neglects the contribution of bound water at the interior surfaces of pores (Weaver et al., 1984). Bound water has a smaller dielectric constant (e.g., $K_{\text{bw}} \approx 6-10$), so that the present estimate of ΔC should be conservative, i.e., an overestimate of the pores' contribution to C . Neglect of the previously mentioned local thickening of the membrane will also contribute to an overestimate of ΔC , because these thicker regions will cause a reduction in capacitance. However, because the dielectric constant of lipid is $K_l \approx 2$ and that of the aqueous pore is $K_2 \approx 80$, the contribution of the pores to ΔC will be far larger than that by local thickened regions. For this reason, the contribution of the thicker lipid regions can be neglected. In this approximation, the total membrane capacitance is the sum of its lipid contribution at fixed thickness, C_l , and of the water-filled pores, C_w .

$$C(t) \approx C_l + C_w = \frac{K_l \epsilon_0 (A_m - A_w(t))}{h} + \frac{K_w \epsilon_0 A_w(t)}{h}; \quad A_m \approx \text{constant} \quad (11)$$

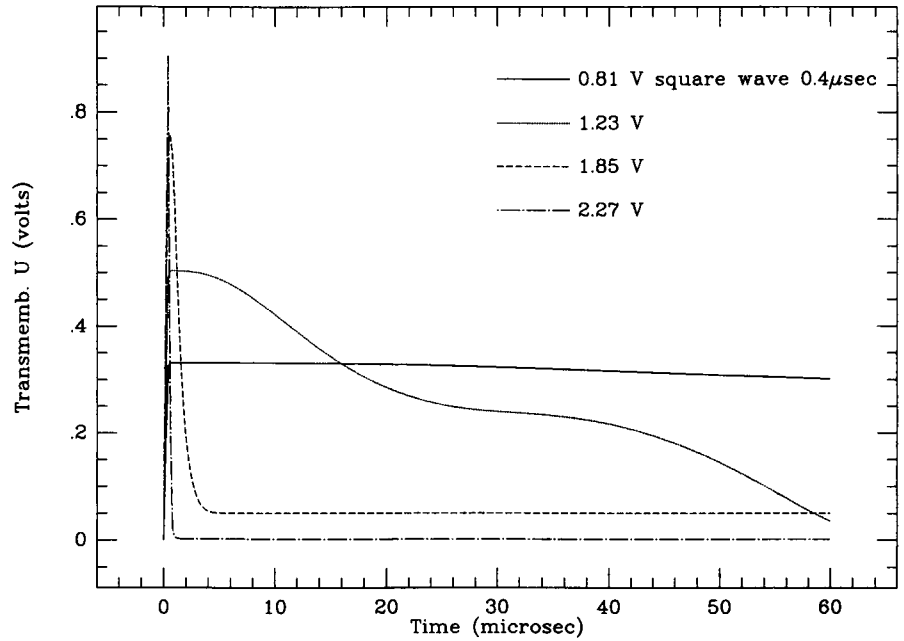
If significant electroporation occurs, the contribution to ΔC may be due mainly to pores. This is in contrast to the situation at small transmembrane voltages where only a few pores are created, and where electrostriction (electrically caused decrease in h) appears to be the dominant mechanism. The fractional change associated with the appearance of pores is

$$\frac{\Delta C(t)}{C} \approx \left(\frac{K_w}{K_l} - 1 \right) \frac{A_w(t)}{A_m} \approx [39] F_w(t) \quad (12)$$

Thus, the time dependence of $C(t)$ due to pores is the same as $F_w(t)$. For this reason, only F_w is presented in Figs. 5, 9, and 13. Multiplication of the maximum value of $F_w(t)$ found there by $K_w/K_l - 1 = 39$ shows that the maximum fractional change in capacitance for reversible electroporation at large transmembrane voltages is less than 2%. We emphasize that these estimates of the pore contribution are overestimates, because the contribution of localized membrane thickening and bound water within pores are both neglected.

The average spacing between pore centers, \bar{S}_{pp} , was estimated by assuming that pore formation occurs randomly with respect to position in the membrane. The area density of pores within the membrane is $\delta_p(t) = N_p(t)/A_m$. We used a polar coordinate system that was fixed at the center of a first pore. The probability of a second pore being located within the

FIGURE 2 Predicted square pulse behavior of the transmembrane voltage, $U(t)$, due to a single $0.4\text{-}\mu\text{s}$ pulse of the indicated amplitudes. As found previously, four distinguishable outcomes are possible: (1) simple charging of the membrane capacitance (smallest pulse; here 0.81 V), (2) rupture of the membrane (larger pulse; here 1.23 V), (3) incomplete reversible electrical breakdown (still larger pulse; here 1.85 V), (4) reversible electrical breakdown (REB) (largest pulse; here 2.27 V). The electrical behavior predicted by a recent transient aqueous pore model (Barnett and Weaver, 1991) agrees reasonably, but not exactly, with experimental observations of these outcomes (Benz et al., 1979).



annulus between s and $s + ds$ from the center of the first pore is

$$P_{1 \text{ in annulus}}(s)ds = 2\pi\delta_p(t)sds \quad (13)$$

where it was assumed that ds is sufficiently small that the probability of finding the center of a second pore in an annulus of thickness ds is much less than unity. This is appropriate because pores are rare events within the membrane. The probability P_1 was multiplied by the probability of finding zero pores in a disk of radius s centered at the first pore. According to Poisson statistics (appropriate for rare events) this second probability is

$$P_{0 \text{ in disk}}(s) = P(n, \bar{n}(s)) = \frac{\bar{n}(s)^n e^{-\bar{n}(s)}}{n!} \quad (14)$$

where $\bar{n}(s)$ is the mean number of pores in a disk of radius s , i.e., $\bar{n}(s) = \delta_p \pi s^2$. The probability of the second pore being located between s and $s + ds$ from the origin, therefore, is given by

$$P(s)ds = P_{0 \text{ in disk}}(s)P_{1 \text{ in annulus}}(s)ds = \frac{(\delta_p \pi s^2)^0 e^{-\pi s^2 \delta_p}}{0!} 2\pi\delta_p s ds \quad (15a)$$

$$= 2\pi\delta_p s e^{-\pi s^2 \delta_p} ds. \quad (15b)$$

To find the mean separation between pore centers, we then computed

$$\bar{S}_{pp}(t) = \int_0^\infty sP(s) ds = 2\pi\delta_p(t) \int_0^\infty s^2 e^{-\pi s^2 \delta_p(t)} ds = \frac{1}{2} \left[\frac{1}{\delta_p(t)} \right]^{1/2}. \quad (16)$$

The largest number of pores, and the smallest pore separation, occurs for pulses that cause REB. In a typical REB simulation, it is predicted that approximately 10^8 pores occur in the membrane of area $A_m = 1.45 \times 10^{-6} \text{ m}^2$, which gives $\delta_p = 1.45 \times 10^{14} \text{ pores m}^{-2}$, and a mean pore spacing of 60 nm . As shown in the figures, during reversible electroporation caused by a short pulse most of the pores are small. Thus, the mean pore spacing is much larger than the diameter of a typical pore. However, during rupture many fewer pores appear, and the behavior is dominated by one or a small number of expanding supracritical pores.

DISCUSSION

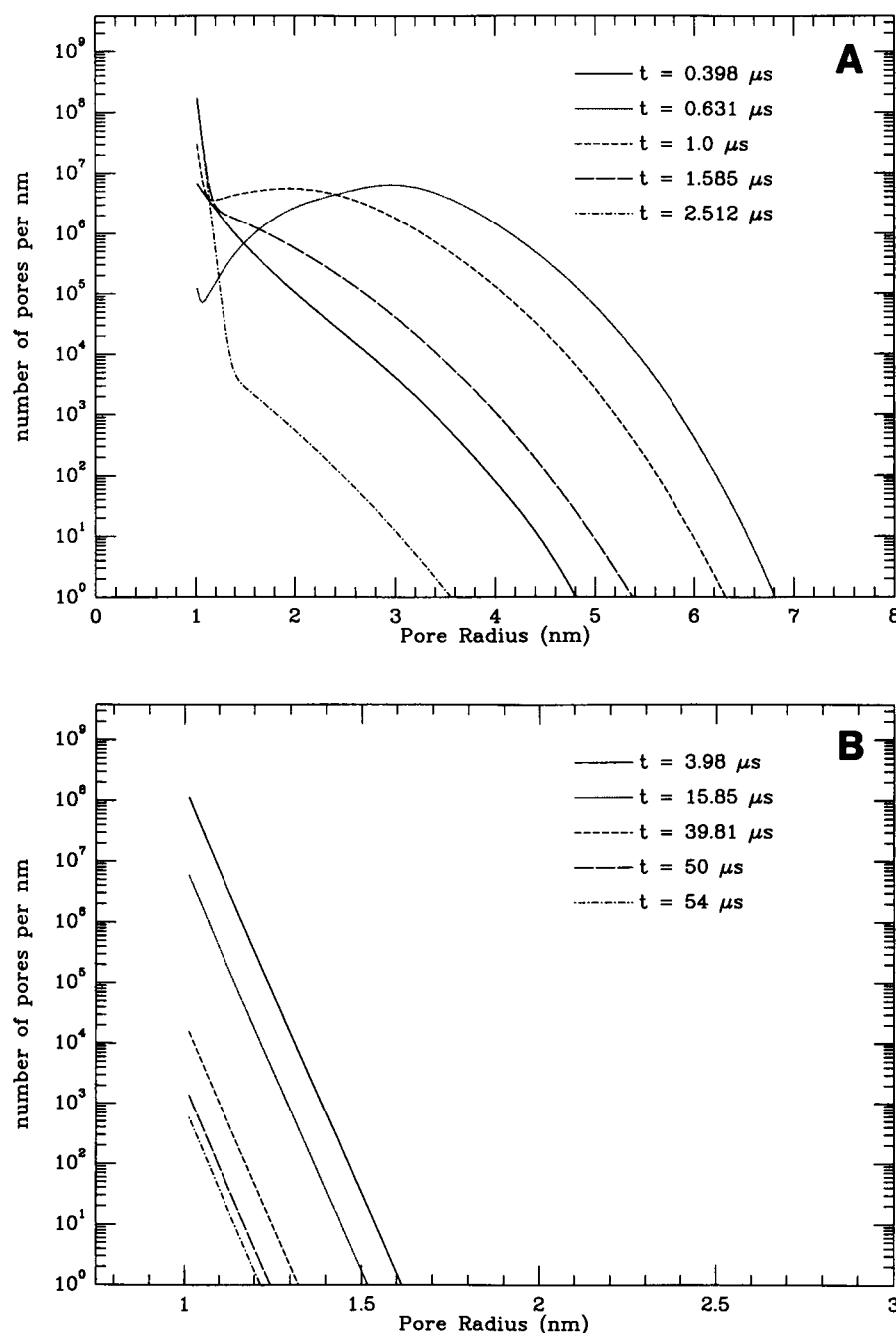
Creation of aqueous pathways ("pores") is central to the concept of electroporation. Such pores are hypothesized to

allow small ions to cross the membrane so that the electrical conduction of the membrane, $G(t)$, can change by orders of magnitude. Although the structure of transient aqueous pores has been suggested in drawings, their actual structure remains unknown. Because of the transient nature of the pores, and the basis of contrast and spatial resolution in known types of microscopy, such pores are not likely to be directly visualized (Weaver, 1993b). Instead, their structure must be inferred. Here we have shown that use of a transient aqueous pore theory that (1) is constructed from continuum physical representations, and (2) is consistent with known electrical behavior of artificial planar bilayer membranes, leads to the view that only a small fraction of the membrane is occupied by pores. This, in turn, places a bound the magnitude of ΔC , and on the minimum value of \bar{S}_{pp} . Similarly, the average spacing of pores was estimated and found to be large, even during reversible electrical breakdown when the largest number of pores are present. Specific predictions of the model are discussed below.

Transmembrane voltage behavior

The model makes specific predictions of $U(t)$, and these have been previously presented (Barnett and Weaver, 1991). The electrical behavior due to a short ($0.4 \mu\text{s}$) square pulse was the subject of an early experimental study using a planar oxidized cholesterol membrane (Benz et al., 1979). As discussed previously, the transient aqueous pore theory predictions are in reasonable agreement with most features of these measurements. Similar planar membrane experiments using exponential and bipolar square pulses apparently have not yet been carried out. Exponential pulses are widely used with cell experiments, but

FIGURE 3 Pore population evolution with time for a typical case involving REB (here the 2.27 V square pulse of Fig. 2). The population is described by a probability density function, $n(r, t)$, such that the number of pores with radii between r and $r + dr$ is $n(r, t)dr$. For the graphs shown here, a finite "bin width" of $\Delta r = 0.026$ nm was used instead of dr . Each of the curves is labeled with the time after the start of the pulse. At $t = 0$ very few (about 6) pores are present. As the pore population evolves because of a pulse, new pores are created at the minimum pore radius, $r_{\min} = 1.0$ nm, and tend to expand because of the reduced pore formation energy at larger U . As inspection shows, for the larger pulses very large numbers of pores are predicted to rapidly appear, with some reaching large (e.g., 4 nm) sizes. Although the rapidly changing pore population distribution cannot be directly observed, it underlies the electrical behavior of Fig. 2. (A) $n(r, t)$ plots for $t = 0.398$ to 2.512 μ s. Note that the plot "peaks" after the 0.4- μ s pulse ends. (B) For $t = 3.98$ – 54 μ s.



usually their time constants are much longer (10^{-4} to 10^{-2} s). Such long pulses have a high probability of rupturing planar membranes and, therefore, are not expected to be particularly worthwhile choices for the planar case. In contrast, vesicles have no meniscus and are not expected to rupture in this way (Sugar and Neumann, 1984), so much longer pulses should be tolerated. The mechanism of cell membrane destruction is less clear. If other cell structures (e.g., cytoskeleton) act to provide boundaries for portions of the membrane, these portions may act like planar membranes and, therefore, be subject to prompt rupture. If not, the cell membrane may behave like a vesicular membrane and not rupture. With this in mind, the planar mem-

brane is relevant to both artificial planar membranes and portions of cell membranes.

Heterogeneous, dynamic pore populations

Although $n(r, t)$ cannot be measured directly, it underlies the functions $U(t)$ and $G(t)$, which can be experimentally determined. Significantly, however, different types of electroporation phenomena appear to be primarily due to different size pores. Specifically, rupture is due to a small number (only one is needed) of large pores, whereas reversible electrical breakdown is due to a large number of small pores. The pore population may also play a sieving role in molecular

FIGURE 4 Predicted mean pore radius as a function of time, $\bar{r}(t)$, for the four square pulse amplitudes of Fig. 2. The density function appearing in Eq. 5 (Fig. 3) was used to compute the arithmetic average value (Eq. 7). Note that \bar{r} changes markedly with pulse amplitude. For small U , the average values are large, but very few pores are present. For example, rupture involves one or a small number of supracritical pores, which can expand until the membrane boundary is reached. At large U , there are many more pores, but most are small. These contribute to the conductance of small ions across the membrane, and underly the protective process of "reversible electrical breakdown," which is really not breakdown, but instead, the onset of massive ionic conductance that discharges the membrane.

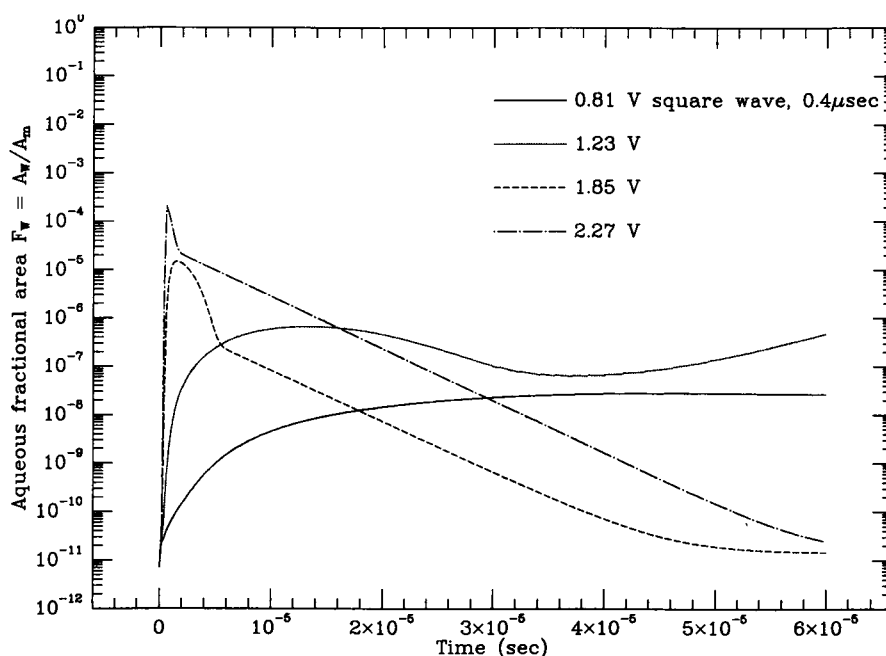
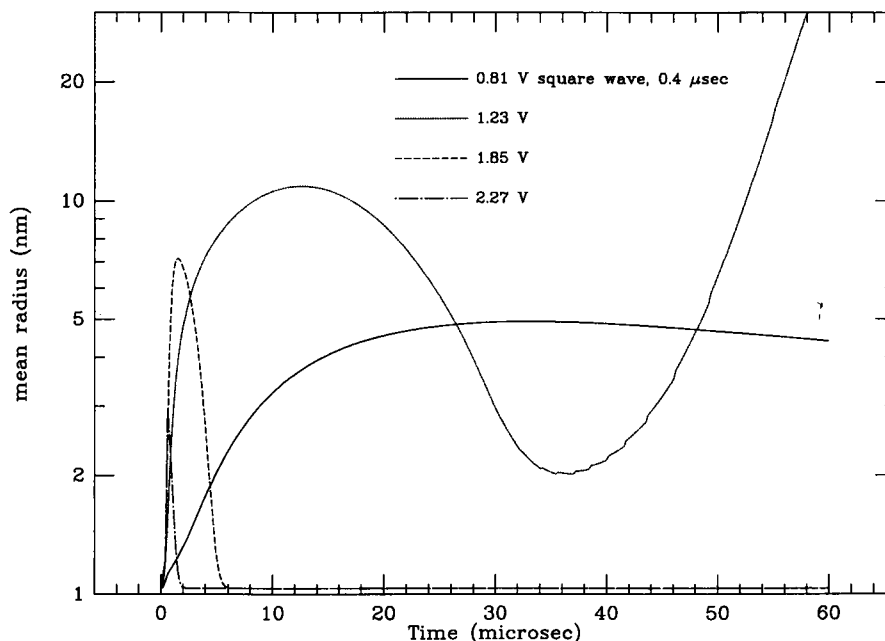


FIGURE 5 Aqueous fractional area of the membrane, $F_w(t) = A_w(t)/A_m$, as a function of time for several different magnitude $0.4 \mu\text{s}$ square pulses. These plots were obtained by computing the pore population distribution (e.g., Fig. 3), summing the individual pore cross sectional areas, $A_p(r) = \pi r^2$, and dividing by the total membrane area, A_m . A realistic value, $A_m = 1.45 \times 10^{-6} \text{ m}^2$, for an artificial planar bilayer membrane was used. Note that the maximum value of F_w is approximately 10^{-3} , i.e., only a small fraction of the membrane is actually occupied pores. Nevertheless, these dominate the transport properties of the membrane, here represented by the massive ionic conductance that is responsible for "reversible electrical breakdown." For pulses that cause REB, the behavior of $F_w(t)$ is nearly the same as $N_p(t)$, the total number of pores (Barnett and Weaver, 1991), because most pores are close to r_{min} . Moreover, the predicted fractional change in membrane capacitance, $\Delta C(t)/C$, exhibits essentially the same behavior as $F_w(t)$, differing only by a proportionality factor (see Eq. 10). As illustrated by the 0.81-V pulse, small pulses cause capacitance changes that are essentially complete within $30 \mu\text{s}$.

transport. If so, the presence of progressively fewer pores at larger radii will play an important role in governing how molecular transport decreases as molecular size increases (Weaver and Barnett, 1992). This suggests that theoretical models that involve only a single size pore will be incomplete and, therefore, misleading.

Mean pore radius behavior

Partial characterization of the pore population during electroporation is obtained by considering the average radius, $\bar{r}(t)$. As shown in Figs. 4, 8, and 12, there are significant changes in the behavior of $\bar{r}(t)$ as the pulse amplitude of

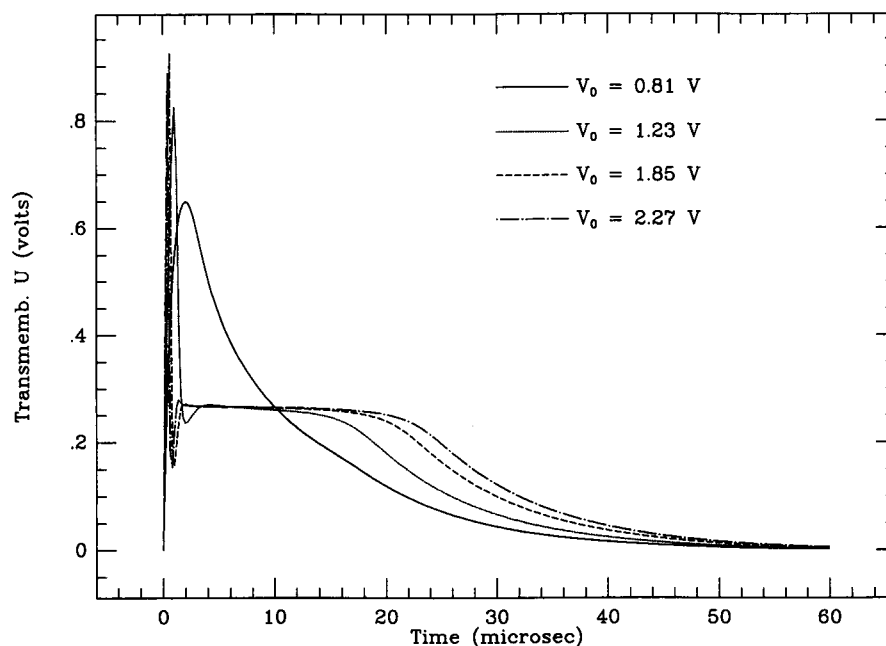


FIGURE 6 Transmembrane voltage, $U(t)$, for four exponential pulses such that $V = V_0 e^{-t/\tau}$ is supplied by the pulse generator (Fig. 1). The same amplitudes, V_0 , as for the square pulses of Fig. 2 were used. Again note that the maximum value of U is about 1 V. The time constant, $\tau = 10 \mu\text{s}$, is considerably larger than the width of the square pulse, so that the membrane is exposed to large U for longer times than in Fig. 2. With this in mind, note the behavior of U the three larger pulses: (1) REB occurs within the first μs , resulting in a sudden drop in U , (2) a resumption of membrane charging then occurs (but the membrane now has a much lower resistance), (3) the same temporary plateau is reached by all three pulses for more than $10 \mu\text{s}$, and a relaxation of U occurs with similar, but not identical, characteristic times. This is not rupture (see Figs. 4 and 5), but a response of the electroporated membrane to decreasing pulses of the different amplitudes. Note the rapid charging, early occurrence of REB (the large "spikes" to the left), and the approximate plateau beginning at about $2 \mu\text{s}$ to about $15\text{--}24 \mu\text{s}$.

the three types of pulses is increased. The evolution of large $\bar{r}(t)$ at moderate U clearly hints at rupture. However, the rapid emergence of small $\bar{r}(t)$ followed by $\bar{r}(t) \rightarrow r_{\min}$, in itself, does not adequately describe reversible electrical breakdown. In general, large increases in U caused by short pulses favor more small than large pores. However, all versions of transient aqueous pore theories to date have used a constant edge energy, γ , although it has been recognized that $\gamma = \gamma(r)$, with a strong r dependence expected for small pores (Weaver and Mintzer, 1981). At least two contributions to γ are neglected in the present models: (1) mechanical strain associated with the effective small pore radius, and (2) coulombic repulsion associated with head groups lining the pore interior. Future versions that use a more realistic $\gamma(r)$ function should predict more larger pores. As further progress towards understanding electroporative molecular transport is achieved, the pore population will probably be found to operate somewhat like a sieve. If so, the distribution of pore sizes will be important. Again, it is clear that a description based on a single pore size is incomplete, because the average pore size usually changes significantly during electroporation.

Fractional aqueous area of the membrane

The transient aqueous pore model predicts that F_w is small for all reversible electroporation phenomena (Figs. 5, 9, and 13). Although dramatic reversible behavior occurs, $F_w(t)$ is

found to be small, never exceeding 10^{-3} , i.e., about 0.1% of the membrane area. In contrast, for irreversible behavior (viz. rupture, a mechanical breakdown), $F_w(t) \rightarrow 1$ as the membrane is destroyed. The small maximum value of $F_w(t)$ emphasizes the idea that minor structural changes within the entire membrane can have significant consequences.

Change in the membrane capacitance

Clearly the membrane capacitance should also change, because aqueous pores have a significantly larger (factor of $K_w/K_m \approx 40$) capacitance per area than nonporated membrane. Thus, it is important to determine whether the transient pore population that is consistent with the dramatic reversible behavior of REB is also consistent with what is known experimentally about the change in capacitance. To our knowledge, there has been only one experimental determination of ΔC under electroporation conditions, for which the capacitance change associated with breakdown of an artificial planar bilayer membrane was found to be less than 2% (Chernomordik et al., 1982). The present theoretical model is in agreement, predicting $[\Delta C/C_0]_{\max} \approx 1$ to 2×10^{-2} during reversible electrical breakdown for the short square, exponential, and bipolar square pulses of Figs. 5, 9, and 13.

Although this approximate agreement for electroporation conditions is important, the transient aqueous pore model should be further tested by comparing (1) the predicted pore

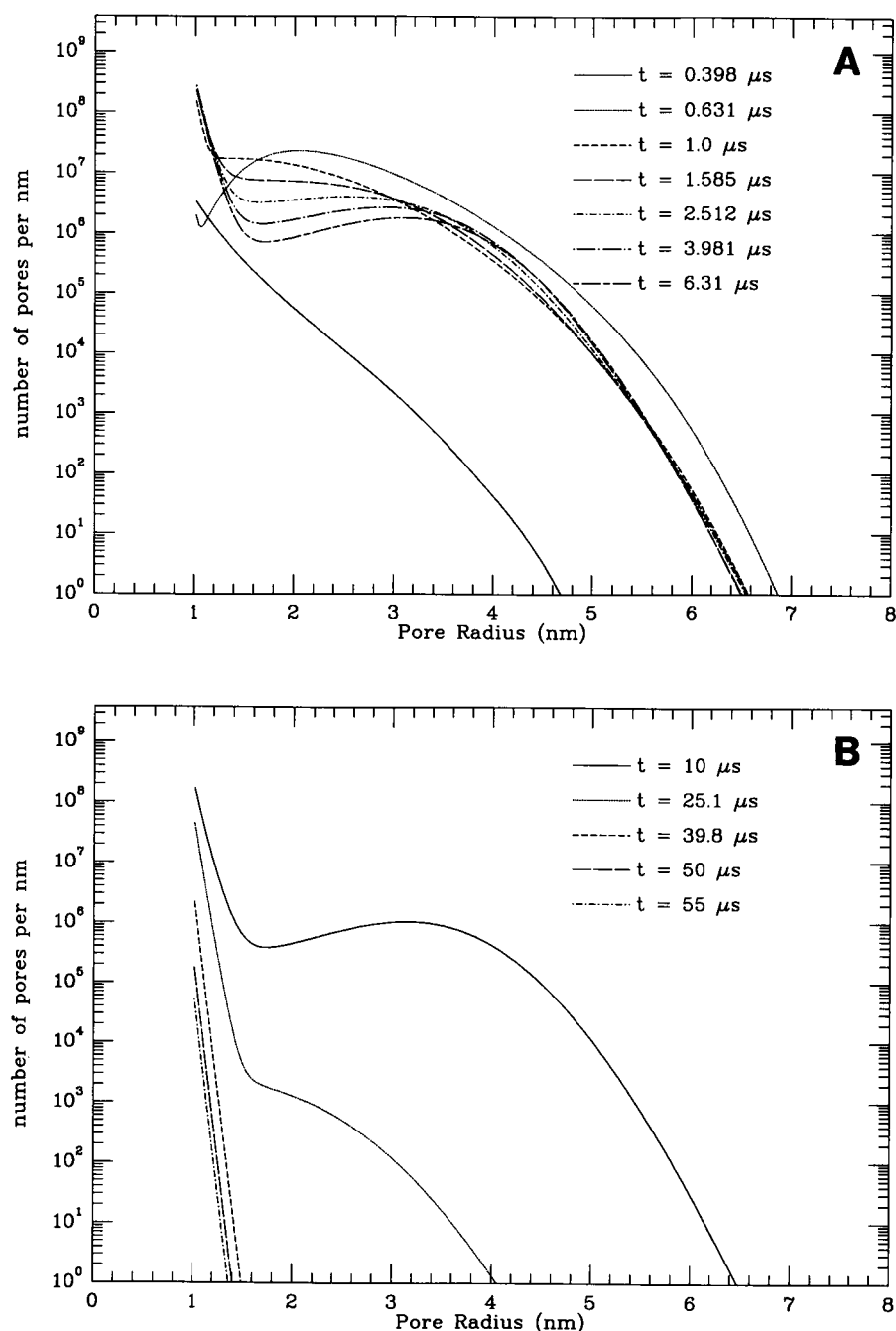


FIGURE 7 Pore population distributions at the indicated times, using the density function, $n(r,t)$ and $\Delta r = 0.026$ nm as in Fig. 3. Note that the probability of having large, supracritical pores that cause rupture remains small. (A) $n(r,t)$ plots for $t = 0.398$ – 6.31 s. Note that the plots do not change significantly over the interval 0.631 – 6.31 μs . (B) For $t = 10$ – 55 μs .

contribution to $\Delta C/C_0$ with (2) the experimental measurements of $\Delta C/C_0$ at low transmembrane voltages that have been interpreted as being due to electrostriction of the entire membrane. At smaller voltages, electrostrictive thinning of the entire membrane has been suggested as the mechanism for capacitance change. For example, measurements by Alvarez and Latorre (1978) found that for U in the range $0 \leq U < 300$ mV, the capacitance of membranes formed from lipids depends on U according to $C(U) = C(0)[1 + \alpha_{AL}U^2]$. Here $C(0)$ is the membrane capacitance at zero transmembrane voltage, and $\alpha_{AL} \approx 0.02$ V $^{-2}$ is the experimentally determined coefficient for “solvent free” bilayers believed to be representative of cell membranes. For $U \approx 0.3$ V, this gives $\Delta C/C_0 \approx 2 \times 10^{-3}$. More recently, measurements by

Toyama et al. (1991) for a more compressible BLM revealed $\Delta C/C_0 \approx 10^{-2}$ at a smaller voltage (150 mV), and this was also attributed to electrostriction. Clearly the transient aqueous pore model is consistent with these results (Table 2), because it predicts a negligible contribution to $\Delta C/C_0$ in the low voltage regime.

Pore-pore separation and pore coalescence

We have also estimated the mean separation of pore centers, \bar{S}_{pp} . These computed results predict that if pores do not interact and, therefore, appear randomly, then pores are widely spaced in a planar membrane for essentially all electroporation phenomena (the exception is rupture, during which the

FIGURE 8 Mean radius, $\bar{r}(t)$, for the four exponential pulses of Fig. 6. Rupture has a low probability, as \bar{r} remains small (cf. Figs. 2–4).

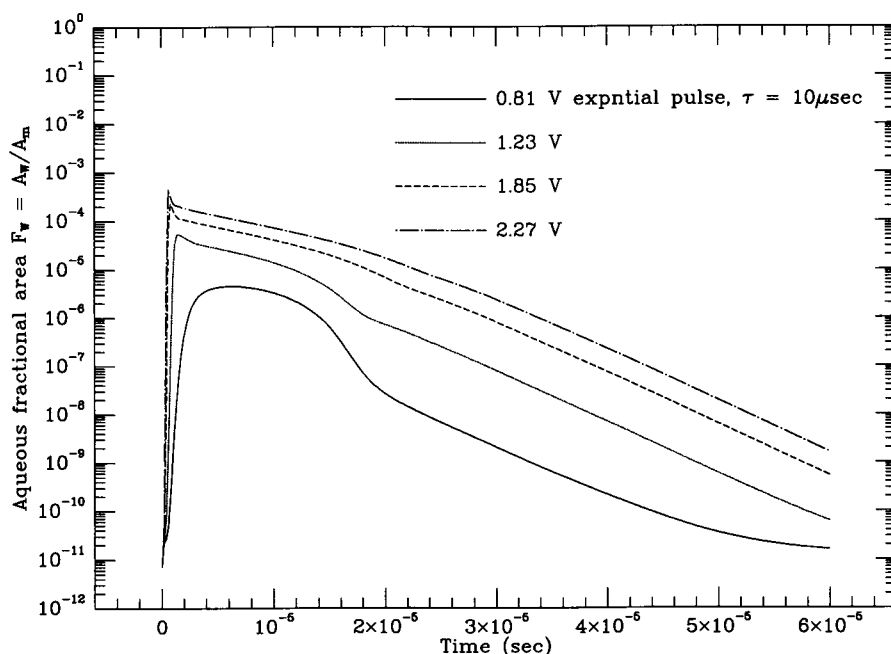
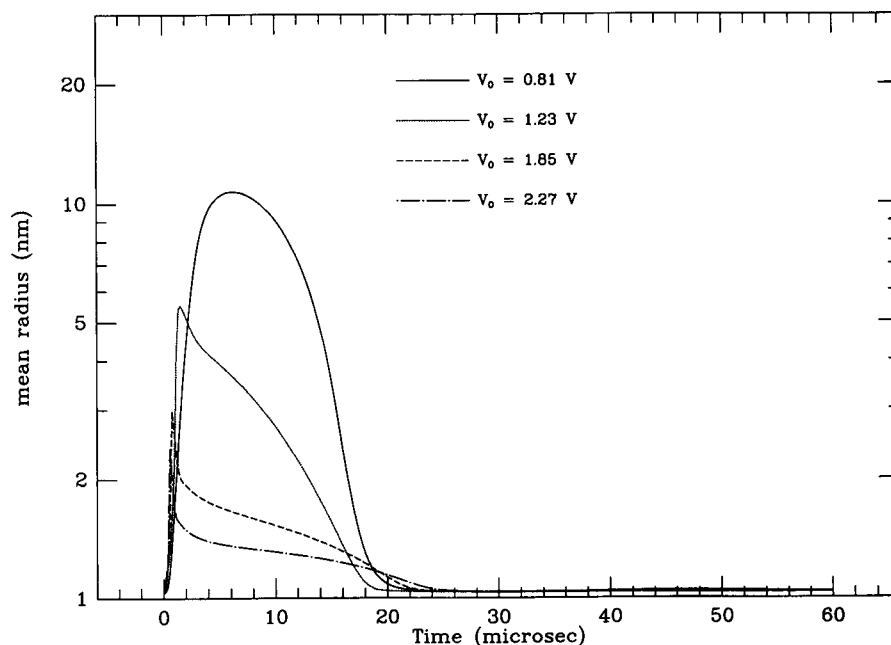


FIGURE 9 Aqueous fractional area, $F_w(t)$, for the exponential pulses of Fig. 6. Again $F_w(t) < 10^{-3}$, even when the largest number of pores occurs (REB).

membrane disappears as one or more pores expand to the membrane's boundary). For small pulses that cause insignificant electroporation, or for the larger pulses that result in a large number of pores, the mean spacing is less than about 30 mean pore diameters. This by itself would suggest that pore-pore encounter and subsequent coalescence is rare in flat membranes, in contrast to the suggested formation of "cracks" (Sugar et. al, 1987) by this mechanism.

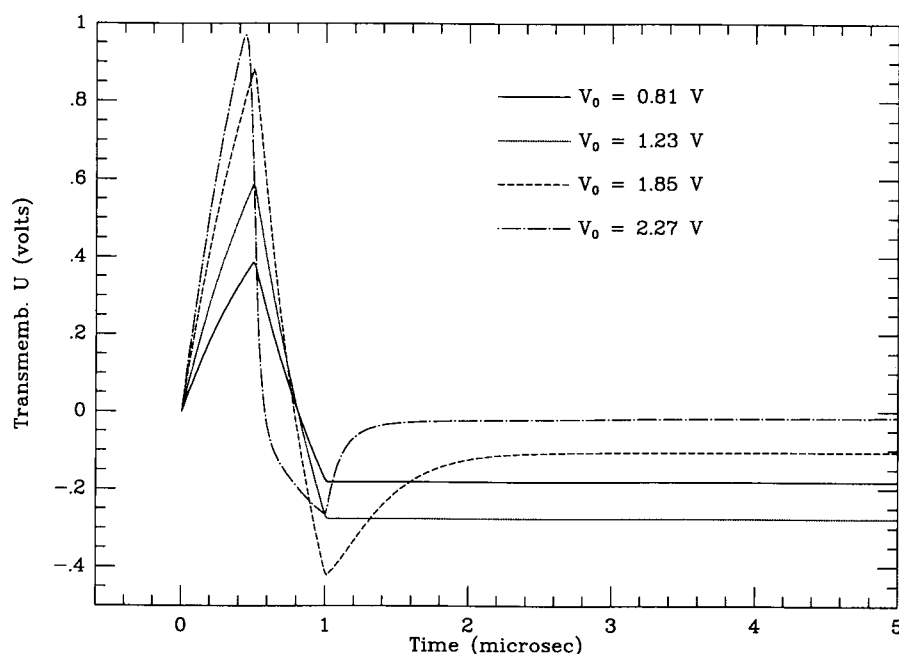
Pore-pore "repulsion" and low probability of close occurrence

Interactions between pores could significantly alter the above prediction. One general type of expected interaction is

through the perturbation of the transmembrane voltage by a conducting pore. A spatially inhomogeneous electric field is expected within the electrolyte near the entrances to a pore (Pastushenko and Chizmadzhev, 1982; Powell et al., 1986; Barnett and Weaver, 1991). For this reason, there is a non-zero component of the electric field parallel to the membrane surface, such that U increases away from a pore. Suppose a first pore exists. Then the probability of forming a second pore will be greatest at sites where U is largest, i.e., a site furthest from the first pore. This qualitative argument thus suggests that pore formation is not entirely random, and that pores will tend to form away from each other.

Moreover, in a flat membrane pores should migrate away from each other. The microscopic fluctuations that cause en-

FIGURE 10 Transmembrane voltage, $U(t)$, for several symmetric bipolar square square pulses that first go positive, and then negative, with a width (time constant) of $1 \mu\text{s}$. For the smaller pulses, the membrane acquires the less conductance, and results in more negatively charged valves at the end of the pulse. As the pulse amplitude is progressively increased, the membrane acquires a larger conductance, and is able to more completely discharge, so that the “final” value of U is progressively closer to zero.



try of high dielectric material (viz. water) into a membrane are larger in regions where U is larger. The “spreading resistance” perturbation of the electric field within the electrolyte due to a first pore results in a gradient in the tangential electric field at the site of a second pore. The contribution to U on the side furthest from the first pore is larger, so aqueous penetration fluctuations at the second pore’s edge away from the first pore will be larger. As a result, the second pore will tend to grow more rapidly on the side away from the first pore and, by this mechanism, will migrate away from the first pore.

Real membranes, however, are not truly flat. Planar membranes are believed to support a variety of shape fluctuations, ranging from waves to indentations and dimples (Chizmadzhev et al., 1979; Bach and Miller, 1980; Lipowsky, 1991). More significantly, cell membranes are curved. In this case, the effect of the resulting tangential component of the electric field should be to cause migration of pores towards the region of larger U . Qualitatively, this could lead to pore-pore contact at the “polar caps” of a spherical cell; this appears to be the dominant mechanism by which pore contact could occur. As suggested previously, this could lead to pore coalescence (Sugar et al., 1987).

Negligible pore-pore magnetic interaction

The magnetic attraction due to current flow through nearly parallel pores will cause a weak attraction. The order of magnitude of this interaction can be estimated by considering two parallel current filaments that correspond to maximum pore currents. The minimum resistance of a small pore is $R_p \approx \rho_{\text{bulk}} h / \pi r_{\text{min}}^2 \approx (0.7 \text{ ohm m}) (2.8 \times 10^{-9} \text{ m}) / (\pi) (1 \times 10^{-9} \text{ m})^2 \approx 10^9 \text{ ohm}$. A typical large transmembrane voltage is of order 1 V, so the maximum pore current is of order 10^{-9} A . The attractive magnetic

force, therefore, is of order $F_{\text{magnetic}} \approx \mu_0 I_{\text{pore}}^2 h / 2\pi S_{\text{pp,min}} \approx (4\pi \times 10^7 \text{ henry m}^{-1}) (10^{-9} \text{ A})^2 (2.8 \times 10^{-9} \text{ m}) / (2\pi) (2 \times 10^{-9} \text{ m}) \approx 3 \times 10^{-25} \text{ N}$. The work done to move one pore a minimal characteristic distance of $S_{\text{pp,min}} = 2r_{\text{min}}$ is used to estimate the associated change in energy, $\Delta W_{\text{magnetic}} \approx 2r_{\text{min}} F_{\text{magnetic}} \approx (2)(10^{-9} \text{ m}) (3 \times 10^{-25} \text{ N}) = 6 \times 10^{-34} \text{ J} \approx 10^{-13} kT$, where $kT = 4 \times 10^{-21} \text{ J}$ is the thermal energy at 37°C . This order of magnitude estimate shows that the magnetic interaction is negligible, even if 100-fold larger pores with 10^4 greater currents (neglecting the spreading resistance) were considered.

SUMMARY

We have estimated properties and behavior of the pore populations that are consistent with the electrical and mechanical behavior due to electroporation in planar bilayer membranes. Except for the irreversible case of rupture at moderate U , only a small fraction ($<10^{-3}$) of the membrane area becomes occupied by aqueous pores. Consistent with this, a rapid but very small change in membrane capacitance is estimated to occur for reversible electroporation. This agrees with experimental evidence and provides justification for the approximation that C is constant in transient aqueous pore theories, here entering through Eq. 6. Finally, because relatively few pores are predicted to appear, the mean pore spacing is large, reaching a minimum of about 60 nm (about 30 minimum pore diameters). Moreover, a qualitative argument that considers the electric field component parallel to the membrane due to a conducting pore suggests that pores are most likely to form away from existing pores, and then to migrate apart. Magnetic attraction of pores is found to be negligible. Together this suggests that flat membranes rarely have pores close together and that pore coalescence in this case is unlikely. However, the opposite is predicted (qualitatively) for

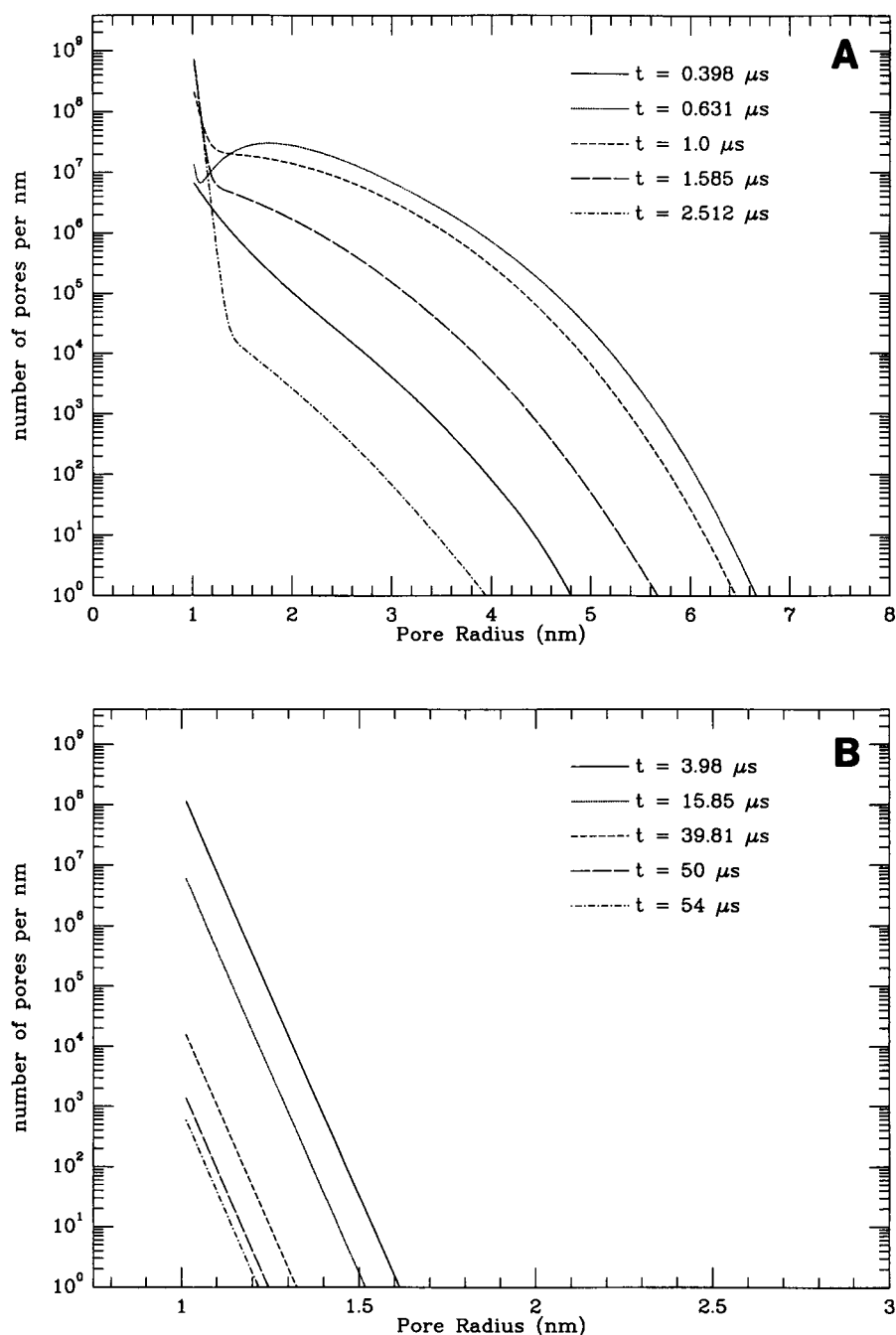


FIGURE 11 Pore population distributions for the case of the bipolar square square pulses. Note that no rupture is predicted. In the present version of the theory, the pore-expanding pressure due to the elevated U is a function of U^2 , so the pore population is enlarged during both the positive and negative portions of the pulse. (A) $n(r,t)$ plots for $t = 0.398$ – $2.52 \mu s$. Note that the population rapidly expands, and has begun collapse (recovery) at $t = 1.0 \mu s$. (B) For $t = 3.98$ – $54 \mu s$.

the curved membranes of cells, for which pores are expected to migrate to the regions with the greatest transmembrane voltage, so that pore coalescence may then occur. For all of the predicted electroporation behavior, it was found that a single pore size does not allow essential aspects of electroporation to be described, because even the average pore size changes significantly. This emphasizes the need to consider explicitly a dynamic, heterogeneous pore population as an integral part of electroporation.

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APPENDIX: ORIGIN OF SOME PARAMETERS

The motivation for some of the model's parameters has not been fully provided in our previous papers. For this reason, we briefly describe the reasoning that led to our currently used values of " a " (coefficient of U^2 in the voltage-dependent component of the barrier to pore creation), δ_c (voltage-independent component of the barrier to pore creation), δ_d (voltage-independent component of the barrier to pore destruction),

FIGURE 12 Mean pore radius, $\bar{r}(t)$, for the bipolar square pulses.

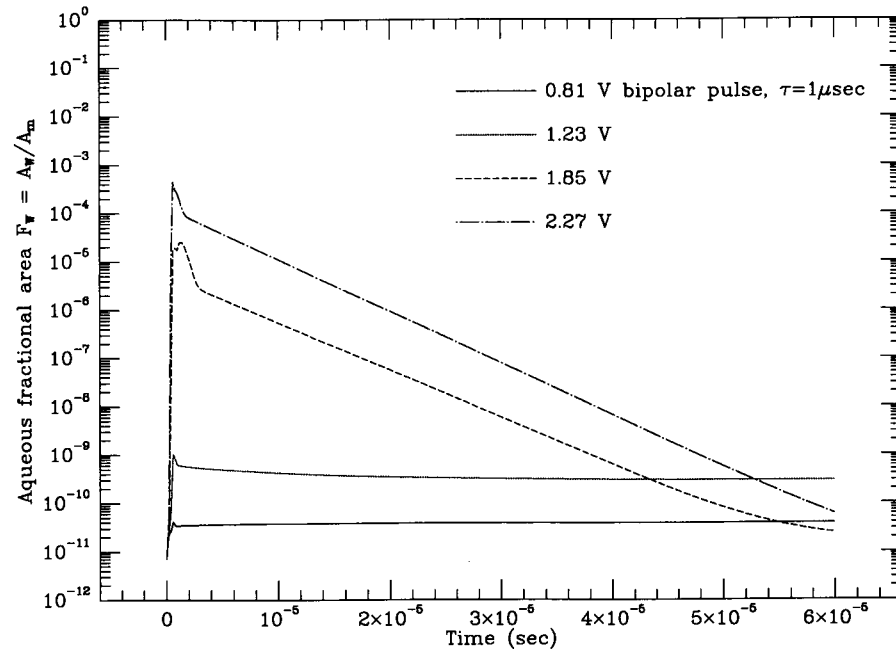
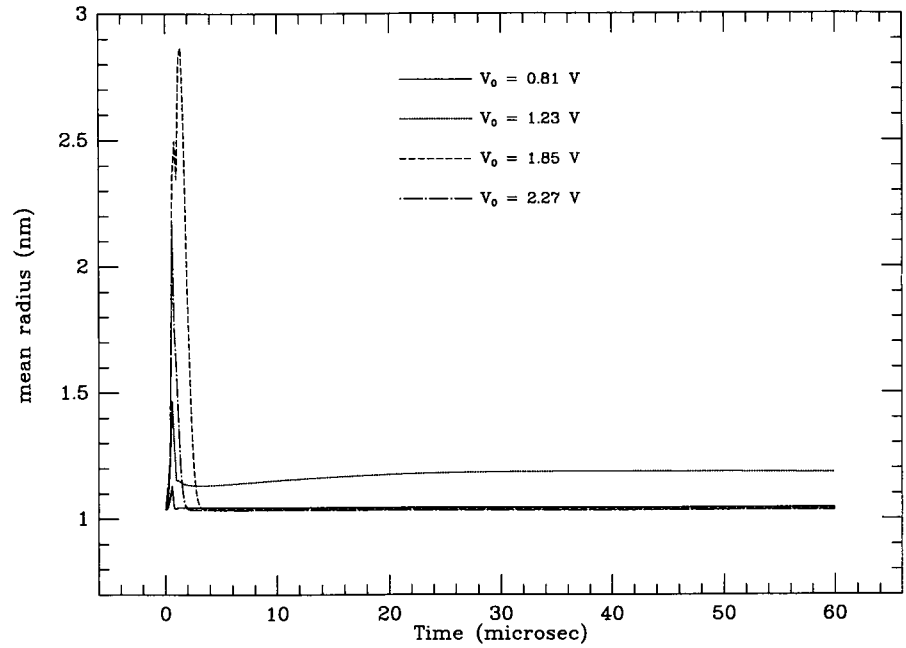


FIGURE 13 Aqueous fractional area, $F_w(t)$ for the bipolar square pulses. Again $F_w(t)$ remains less than 10^{-3} .

$\nu_0 = \nu/V_m = \nu/A_m h$ (ν_0 is the attempt rate density, and ν is the corresponding prefactor of the Boltzmann factor containing δ_c), χ (prefactor of Boltzmann factor containing δ_d), and D_p (diffusion constant in pore radius space). It is emphasized that although the simulation exhibits several key features of electroporation (simple membrane charging, rupture, incomplete REB, and then REB as the pulse magnitude is increased), it is not entirely accurate. Furthermore, as noted previously (Barnett and Weaver, 1991), given the multiparametric nature of the model and the relative lack of quantitative experimental data available, it is not presently realistic to seek parameter values by numerical fits. With these limitations in mind, the introduction of these particular parameters, and the selection of their numerical values, should be regarded as approximate and illustrative, rather than definitive.

A starting point for obtaining these parameters considers the steady state at zero transmembrane voltage. Specifically, we assume that an artificial planar bilayer membrane at $U = 0$ has a time average number of pores, \bar{N} , which is small. The actual number is not known, so a plausibly small value, of order 10, was chosen. We did not want $\bar{N} \leq 1$, because experience in working with the highly nonlinear simulation had shown us that key electroporation-related phenomena would not then readily occur. Our approach was to consider the steady state at $U = 0$, and to then find values of δ_c , δ_d , χ , and ν_0 that were individually plausible, and that also allowed the model to exhibit basic electroporation behavior when used with a range of short voltage pulses. A lengthy series of simulation trials with short square pulses was then used to guide further the choice of all the parameter values.

TABLE 2 Illustrative Fractional Capacitance Changes

Pulse type	$[\Delta C/C_0]_{\max}$	Phenomenon
2.27 V, 0.4 μ s square	1×10^{-2}	Reversible discharge to zero (Fig. 2)
2.27 V, 10 μ s exponential	2×10^{-2}	Reversible discharge to zero (Fig. 6)
2.27 V, 1 μ s bipolar square	2×10^{-2}	Reversible discharge to zero (Fig. 10)
0.35 V, 50 μ s square	1×10^{-5}	Steady 0.35 V achieved*
0.20 V, 50 μ s square	2×10^{-9}	Steady 0.20 V achieved*

* Conditions of negligible electroporation, i.e., creation of only a few pores and, therefore, insignificant pore-related conduction to provide discharge of the membrane on a rapid time scale. Under these conditions, the main contribution to ΔC is believed to be electrostriction (Alvarez and Latorre, 1978; Toyama et al., 1991). These predicted steady values of $[\Delta C/C_0]$ due to pores were computed by using a 50 μ s square pulse in the simulation, which resulted in the membrane achieving $U = 0.35$ and 0.20 V, respectively. Note that 50 μ s is considerably longer than needed to achieve a steady state (see Fig. 2 for the 0.81-V pulse). The significance of these two smaller, 50- μ s pulses is that the transient aqueous pore model predicts achievement of steady changes that are significantly smaller than the experimental observations in this range. For example, Alvarez and Latorre found $[\Delta C/C_0] \approx 2 \times 10^{-4}$ at $U \approx \pm 0.1$ V (Alvarez and Latorre, 1978), and Toyama et al. (1991) found $[\Delta C/C_0] \approx 2 \times 10^{-3}$ to 10^{-2} at $U \approx \pm 0.15$ V. In the low voltage region, these experimental values are much larger than the predicted pore contribution, which demonstrates that the pore model does not violate experimental observations in the low voltage, nonelectroporation region.

The steady-state probability density function, $n(r)$, is obtained by setting the left side of Eq. 5 equal to zero. A solution of the resulting ordinary differential equation is

$$n(r) = n_0 e^{-\Delta E/kT}, \quad (A1)$$

This function is a Boltzmann factor multiplied by a normalization constant, and it describes the distribution of pore sizes for any constant transmembrane voltage (Weaver et al., 1984). It is like a "law of atmospheres," in that the probability of finding an entity (here a pore) decreases exponentially as the entity energy increases, with only thermal fluctuations available to populate the system.

We next use the $U = 0$ case to aid in selection of the basic parameters that govern pore creation and destruction. At $U = 0$ the contribution of the membrane surface energy, Γ , is small compared to that of the edge energy, γ . This is a consequence of the "barrier" (maximum value of $\Delta E(r, U = 0)$) being large, so that the probability of having a large pore is extremely small, and is consistent with the interpretation that rupture at $U = 0$ is negligible. In this case only the first term in Eq. 1 is significant, and ΔE can be linearized to $\Delta E \approx 2\pi\gamma r$. This means that

$$n(r) \approx n_0 e^{-2\pi\gamma r/kT} = n_0 e^{-r/\lambda_r}, \quad (A2)$$

where $\lambda_r = kT/2\pi\gamma \approx 3 \times 10^{-11}$ m is a characteristic length in pore radius space. The small size of λ_r means that at zero transmembrane voltage the pore population falls off extremely rapidly with increasing r . Therefore, all of the pores at $U = 0$ have $r \approx r_{\min}$. This, in turn, justifies our approximating Eq. 1 by only the first term.

We can now find an expression for the number of time average pores, \bar{N} , in a particular planar membrane by integrating $n(r)$ from r_{\min} to ∞ .

$$\bar{N} = \int_{r_{\min}}^{\infty} n_0 e^{-r/\lambda_r} dr = n_0 \lambda_r e^{-r_{\min}/\lambda_r} \quad (A3)$$

To proceed, n_0 must be determined. Clearly the average number of pores present is determined by a balance between pore creation and destruction.

Eq. 4, which describes pore destruction, involves the factor

$$n(r_{\min}) = n_0 e^{-r_{\min}/\lambda_r}. \quad (A4)$$

The steady-state condition of balance of creation and destruction is simply $(\dot{N})_c = (\dot{N})_d$, which at $U = 0$ becomes

$$\nu e^{-\delta_c/kT} = \chi n(r_{\min}) e^{-\delta_d/kT} = \chi n_0 e^{-r_{\min}/\lambda_r} e^{-\delta_d/kT}. \quad (A5)$$

As shown in the main part of this paper, for reversible electroporation involving many pores at large U , the pores are always widely spaced. At $U = 0$ the few pores present are essentially independent. Thus, if we think of the pore creation and destruction as being governed by a transition from a "zero pore state" for the entire membrane to a "one pore state," we expect that the barrier for a " $0 \rightarrow 1$ " transition (δ_c) will be larger than the barrier for a " $1 \rightarrow 0$ " transition (δ_d). It is generally believed that pore creation proceeds by first forming hydrophobic pores, followed by surmounting a large barrier to create a minimum size hydrophilic pore (Abidor et al., 1979). In fact, at $U = 0$ both δ_c and δ_d are believed to be large compared to their difference, $\delta_c - \delta_d$. For simplicity, therefore, we have assumed that the same barrier height governs both the " $0 \rightarrow 1$ " and " $1 \rightarrow 0$ " transitions, and we have accounted for the difference in barrier heights through their very different prefactors ν and χ (see below). That is, for convenience we have assumed that $\delta_c = \delta_d$, and we have incorporated the rate difference into the values of the corresponding barrier prefactors, ν and χ . With this simplification, Eq. A5 becomes

$$\nu = \chi n_0 e^{-r_{\min}/kT}. \quad (A6)$$

We next consider the relationship between ν and χ . The relative magnitudes of ν and χ can be estimated by arguing: (1) that creation of a pore can occur essentially anywhere in the membrane, because only a small fraction of the membrane area is occupied by pores, and (2) the destruction of a pore is a highly localized event. This means that creation events can involve fluctuations within the entire volume of the membrane, whereas destruction events must be localized to a much smaller volume, one that is typical of the membrane molecules associated with a pore of radius r_{\min} . More specifically, we argue that the order of magnitude ratio is

$$\frac{\chi}{\nu} \approx \frac{2\pi r_{\min}(\delta r)h}{A_m h} \approx \frac{2\pi r_{\min}^2}{A_m} \approx 5 \times 10^{-12}, \quad (A7)$$

where $(\delta r) \approx r_{\min}$ is an estimator of the radial extent of an annular volume having fluctuations that can destroy a pore. The significant inequality implied by Eq. A7 also suggests that minimum size pores will require much longer times for their destruction than for their creation, i.e., that pores may have relatively long lifetimes. This is consistent with the observations of Chizmadzhev and co-workers, who find that pores, which are believed to be near the minimum size, have lifetimes of many seconds (Abidor et al., 1979).

We now find \bar{N} by recognizing that the steady state is independent of kinetics, because only the ratio ν/χ is important, and we write n_0 as

$$n_0 = \left[\frac{\nu}{\chi} \right] e^{+r_{\min}/kT} \approx 1.2 \times 10^{24} \text{ m}^{-1}. \quad (A8)$$

Substitution into Eq. A2 yields $\bar{N} \approx 7$, which is consistent with the assumed constraint that fewer than 10 pores should be present at $U = 0$. This result can also be obtained using the exact expression given in Eq. 28 in Barnett and Weaver (1991).

A major goal of the simulation is to describe dynamic behavior, and this is significantly more difficult than treating the steady state. Given our assumptions and approximations, there remain three undetermined parameters that directly enter into the description of pore creation and destruction. There is (1) a single voltage-independent barrier ($\delta_c = \delta_d$), (2) a voltage-dependent barrier component for pore creation (aU^2 in $\Lambda = \delta_c - aU^2$), and (3) one prefactor (ν), because the ratio ν/χ is fixed by Eq. A7. A fourth parameter, D_p , the diffusion constant in pore radius space, only indirectly affects pore creation and destruction.

With this in mind, we next consider the parameter “ a ” in aU^2 . Equation 3 describes the pore creation rate, $(\dot{N})_c$, in terms of a Boltzmann factor and an attempt rate (prefactor). The energy barrier of the Boltzmann factor, $\Lambda = \delta_c - aU^2$, contains both a voltage-independent component and a voltage-dependent component. The total barrier to pore creation, $\Lambda = \delta_c - aU^2$, is expected to be much larger than the pore energy for a minimum size pore ($r = r_{\min}$). For simplicity we assumed the form $\Lambda = \delta_c - aU^2$ and used the constraint $\Lambda > \Delta E(r_{\min}, U)$. The origin of the value $\delta_c = 2 \times 10^{-19}$ J was mentioned above. We then used an order of magnitude estimate for “ a ” by considering the order of magnitude of the energy aU^2 for a pore size intermediate to the minimum hydrophilic pore size ($r_{\min} = 1$ nm) and the hydrophobic pores (radii of zero up to r_{\min} ; Abidor et al., 1979). Specifically, we used $r_{\text{intermediate}} = 0.16$ nm, which corresponds to the value

$$a = \frac{\epsilon_0(K_w - K_l)\pi r_{\text{intermediate}}^2}{h} \approx 1.9 \times 10^{-20} \text{ F}, \quad (\text{A9})$$

which is a capacitance associated with this size hypothetical intermediate (transitional state) hydrophobic pore.

Once created, however, pores also expand and contract according to Eq. 5, for which the relevant parameter is D_p and which, through the Einstein relation, can also be considered as a mobility in radius space (Powell and Weaver, 1986). The remaining three parameters were obtained by considering both order of magnitude estimates of possible magnitudes, and by carrying out many simulations of electroporation dynamics. First we consider δ_c in the context of Eq. 3. The minimum energy to make a pore of radius r_{\min} is $\Delta E(r_{\min}, U)$. Inspection of Eq. 1 shows that the voltage-independent component of ΔE is the minimum possible value for δ_c , viz.

$$(\delta_c)_{\min} = 2\pi\gamma r_{\min} - \pi\Gamma r_{\min}^2 = 1.2 \times 10^{-19} \text{ J} = 30 \text{ kT}. \quad (\text{A10})$$

However δ_c must be larger than this value, because $(\delta_c)_{\min}$ does not take into account the the assumed transition of a hydrophobic pore to a hydrophilic pore, which is unknown but believed to be significant (Abidor et al., 1979; Glaser et al., 1988). Therefore, somewhat arbitrarily but also using simulation trial results, the value $\delta_c = 2 \times 10^{-19}$ J = 50 kT was chosen.

The attempt rate density was originally estimated by considering only the molecules of a fluid membrane and treating these molecules as a dense ideal gas. This gave an order of magnitude estimate, $\nu_0 \approx 2 \times 10^{38} \text{ s}^{-1} \text{ m}^{-3}$ (Weaver and Mintzer, 1981). Subsequently, it was recognized that ν_0 could be expressed in terms of other model parameters (Powell and Weaver, 1986), which led to another estimate, $\nu_0 \approx 5 \times 10^{32} \text{ s}^{-1} \text{ m}^{-3}$. As noted there, the large (almost six orders of magnitude) difference is not actually significant, because it multiplies a Boltzmann factor. In the present paper we carried out lengthy exploration of the simulation for many square pulse magnitudes, and in the process we found that the presently used value $\nu_0 = \nu/\lambda_{\text{mb}} \approx 2 \times 10^{42} \text{ s}^{-1} \text{ m}^{-3}$ resulted in successful simulation of electroporation behavior. However, a rigorous basis for ν_0 is still lacking.

The remaining parameter whose value needs explanation is the currently used value $D_p = 5 \times 10^{-14} \text{ m}^2 \text{ s}^{-1}$. The diffusion constant in pore radius space was originally introduced for electroporation by Chizmadzhev and his co-workers in their 1979 series of papers (Abidor et al., 1979). In one of our earlier papers (Powell and Weaver, 1986), an order of magnitude estimate of the magnitude was made by treating liquid water as a dense ideal gas, but there was no attempt to include the effect of water's viscosity. This gave the value $D_p = 1.1 \times 10^{-12} \text{ m}^2 \text{ s}^{-1}$. However, the effect of viscosity should be to slow transport processes and, therefore, to yield a smaller value. In the current version of the model (Barnett and Weaver, 1991), a 20-fold smaller value of $D_p = 5 \times 10^{-14} \text{ m}^2 \text{ s}^{-1}$ was used, again based partly on many simulation results.

In summary, the introduction of the particular parameters, and the selection of their numerical values, is based on plausible physical constraints and on the results of many simulation trials. The parameters that can be obtained using steady-state behavior are generally better understood than those that are intimately involved in the dynamic behavior. In all cases, it is important to recognize that relatively little quantitative information is available regarding detailed electroporation behavior and, therefore, that the simulation should be regarded as approximate and illustrative, not definitive.

We believe that although it is significant that the simulation can describe quantitatively some essential features of electroporation, much more remains to be done.

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